$$+ 3y^{2}I_{6} + i \frac{y}{a} \{3a^{2}(I_{2} - I_{1}) + 3az_{j}(I_{3} - I_{4}) - 3x^{2}I_{7}$$

$$+ y^{2}I_{5}\} \} - \frac{6c_{66}P_{z}}{a^{4}} G_{0} \{fa[x\psi_{1}(\xi_{0}) + iy\psi_{2}(\xi_{0})]$$

$$- \bar{f} \left[\frac{x}{a} \{3a^{2}(I_{9} - I_{2}) + 3az_{0}(I_{4} - I_{8}) - x^{2}I_{10} + 3y^{2}I_{6}\}$$

$$+ i \frac{y}{a} \{3a^{2}(I_{2} - I_{1}) + 3az_{0}(I_{3} - I_{4}) - 3x^{2}I_{7} + y^{2}I_{5}\} \} \},$$

$$\sigma_{zm} = \frac{6P_{z}}{a^{3}} \sum_{j=1}^{3} G_{j}\omega_{mj}[xf_{x}\psi_{1}(\xi_{j}) + yf_{y}\psi_{2}(\xi_{j})],$$

$$T_{zm} = \frac{3P_{z}}{a^{4}} \sum_{j=1}^{3} G_{j}s_{j}\omega_{mj}[faz_{j}\psi_{3}(\xi_{j}) - \bar{f} [az_{j}\{\psi_{1}(\xi_{j}) - \psi_{2}(\xi_{j})\}$$

$$- a^{2}(I_{11} - I_{12}) + x^{2}I_{8} - y^{2}I_{3}$$

$$+ i2xyI_{4}] \} - \frac{3P_{z}}{a^{4}} G_{0}s_{0}\rho_{m}\{faz_{0}\psi_{3}(\xi_{0}) + \bar{f} [az_{0}\{\psi_{1}(\xi_{0})$$

 $-\psi_2(\xi_0) - a^2(I_{11} - I_{12}) + x^2I_8 - y^2I_3 + i2xyI_4] \} (15)$ 

where  $e, \xi_i (j = 0, 1, 2, 3)$  and  $F(\varphi_i, e) (j = 0, 1, 2, 3)$  are the same as those in Eq. (11);  $\psi_k$  (k = 1, 2, 3),  $I_{11}$ ,  $I_{12}$ , and  $I_l$  (l = 1, 2, 3, ... 12) are listed in Appendices A and B in Hanson and Puja (1997).

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#### References

Bryant, M. D., and Keer, L. M., 1982, "Rough Contact Between Elastically and Geometrically Identical Curved Bodies," ASME JOURNAL OF APPLIED MECHANICS, Vol. 49, pp. 345-352.

Ding, H. J., Chen, B., and Liang, J., 1996, "General Solution for Coupled Equations for Piezoelectric Media," Int. J. Solids Structures, Vol. 33, pp. 2283-2298.

Ding, H. J., Hou, P. F., and Guo, F. L., 1998, "The Elastic and Electric Fields for Three-Dimensional Contact for Transversely Isotropic Piezoelectric Materials," Int. J. Solids Structures, accepted for publication.

Fabrikant, V. I., 1989, Applications of Potential Theory in Mechanics, Selection of New Results, Kluwer Academic Publishers, Dordrecht, The Netherlands.

Fabrikant, V. I., 1991, Mixed Boundary Value Problems of Potential Theory and Their Applications in Engineering, Kluwer Academic Publishers, Dordrecht, The Netherlands.

Fan, H., Sze, K. Y., and Yang, W., 1996, "Two-Dimensional Contact on a Piezoelectric Half-Space," Int. J. Solids Structures, Vol. 33, pp. 1305–1315.

Gladwell, G. M. L., 1980, Contact Problems in the Classical Theory of Elasticity, Sijthoff & Noordhoff, Alpen aan den Rijn, The Netherlands.

Haines, D. J., and Ollerton, E., 1963, "Contact Stress Distributions on Elliptical Contact Surfaces Subjected to Radial and Tangential Forces," Proc. Instn. Mech. Engrs., Vol. 177, pp. 95-114.

Hanson, M. T., and Puja, I. W., 1997, "The Elastic Field Resulting From Elliptical Hertzian Contact of Transversely Isotropic Bodies: Closed-Form Solutions for Normal and Shear Loading," ASME JOURNAL OF APPLIED MECHANICS, Vol. 64, pp. 457--465.

Johnson, K. L., 1985, Contact Mechanics, Cambridge University Press, Cambridge, UK.

Sackfield, A., and Hills, D. A., 1983a, "Some useful Results in the Classical Hertz Contact Problem," Journal of Strain Analysis, Vol. 18, pp. 101-105.

Sackfield, A., and Hills, D. A., 1983b, "Some useful Results in Tangentially Loaded Hertzian Contact Problem," Journal of Strain Analysis, Vol. 18, pp. 107-110.

Sackfield, A., Hills, D. A., and Nowell, D., 1993, "The Stress Field Induced by a General Elliptical Hertzian Contact," ASME Journal of Tribology, Vol. 115, pp. 705-706

Sosa, H. A., and Castro, M. A., 1994, "On Concentrated Loads at the Boundary of a Piezoelectric Half-Plane," J. Mech. Phys. Solids, Vol. 42, pp. 1105-1122.

Wang, Z., and Zheng, B., 1995, "The General Solution of Three-Dimensional Problems in Piezoelectric Media," Int. J. Solids Structures, Vol. 32, pp. 105-115.

Willis, J. R., 1966, "Hertzian Contact of Anisotropic Bodies," J. Mechanics and Physics Solids, Vol. 14, pp. 163–176. Willis, J. R., 1967, "Boussinesq Problem for an Anisotropic Half-space," J.

Mechanics and Physics Solids, Vol. 15, pp. 331-339.

# **Exact Eshelby Tensor for a Dynamic Circular Cylindrical Inclusion**

## Z.-Q. Cheng<sup>1</sup> and R. C. Batra<sup>2</sup>

## 1 Introduction

This work is motivated by Mikata and Nemat-Nasser's (1990) study of dynamic transformation toughening of ceramics in which a typical dynamic problem of a spherical inclusion was solved. Mikata and Nemat-Nasser (1990, 1991), Mikata (1993), and Cheng and He (1996) have obtained exact analytic solutions for a dynamic spherical inclusion embedded in an infinite linear elastic and isotropic medium. However, the corresponding dynamic problem of a circular cylindrical inclusion has not been studied. Mura (1988) and Mura et al. (1996) have reviewed the literature on inclusion problems.

The time-harmonic elastic field caused by an infinitely long circular cylindrical inclusion is obtained in this paper, and a closed-form expression is derived for the dynamic Eshelby tensor. Unlike the static case, the Eshelby tensor for the dynamic problem is not uniform even at interior points within the circular cylinder. In the limit of quasi-static deformations the present solution reduces to Eshelby's results.

#### 2 Analysis

Following Eshelby (1957, 1959) and Mura (1982), an inclusion is referred to a subset of a matrix that has a prescribed eigenstrain (or transformation strain) and has the same elastic properties as the matrix. Consider the following time-harmonic eigenstrain

\*/

$$e_{kl}^{*}(\mathbf{x}, t) = e_{kl}^{\Omega}(\mathbf{x})\Lambda(\Omega)e^{-i\omega t},$$
  

$$\Lambda(\Omega) = \begin{cases} 1, & \mathbf{x} \in \Omega\\ 0, & \mathbf{x} \in R^{3} - \Omega \end{cases}$$
(1)

where  $\Omega$  is the region occupied by an inclusion that is embedded in an infinite (i.e.,  $R^3$ ) isotropic, linear elastic medium, and  $\omega$ denotes an angular frequency. It is assumed that a time-harmonic eigenstrain will induce time-harmonic displacement, strain, and stress fields. Henceforth we omit the factor  $exp(-i\omega t)$ . Also, a comma followed by a subscript *i* denotes a partial derivative with respect to the rectangular Cartesian coordinate  $x_i$ , a repeated index implies summation over the range of the index, Latin subscripts range over 1, 2, 3 and Greek subscripts over 1 and 2.

Equations for determining the displacement field in steady-state deformations of a linear elastic isotropic body are

$$\sigma_{ij,i} + \rho \omega^2 u_i = 0, \quad \sigma_{ij} = C_{ijkl} [e_{kl} - e_{kl}^{\Omega} \Lambda(\Omega)],$$

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## **BRIEF NOTES**

$$e_{kl} = \frac{1}{2} \left( u_{k,l} + u_{l,k} \right), \tag{2}$$

where  $\rho$  is the mass density,

$$C_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}), \qquad (3)$$

 $\lambda$  and  $\mu$  the Lamé constants and  $\delta_{ij}$  the Kronecker delta. The corresponding displacement field can be expressed as (Mura, 1982)

$$u_i(\mathbf{x}) = -\int_{\Omega} C_{jlmn} e_{mn}^{\Omega}(\mathbf{x}') g_{ij,l}(\mathbf{x} - \mathbf{x}') d\mathbf{x}', \qquad (4)$$

where  $g_{ij}$  is the Green function defined by

$$g_{lm}(\mathbf{x} - \mathbf{x}') = \frac{1}{4\pi\rho\omega^2} \times \left[\beta^2 \delta_{lm} \frac{e^{i\beta r}}{r} - \frac{\partial^2}{\partial x_l \partial x_m} \left(\frac{e^{i\alpha r}}{r} - \frac{e^{i\beta r}}{r}\right)\right], \quad (5)$$

$$r^{2} = (x_{k} - x_{k}')(x_{k} - x_{k}'), \quad \alpha^{2} = \frac{\rho\omega^{2}}{\lambda + 2\mu}, \quad \beta^{2} = \frac{\rho\omega^{2}}{\mu}.$$
 (6)

If  $e_{nn}^{\Omega}(\mathbf{x})$  in Eq. (1) is constant over  $\Omega$ , then the displacement and strain can be expressed as (Mikata and Nemat-Nasser, 1990)

$$u_i(\mathbf{x}) = J_{ikl}(\mathbf{x})e_{kl}^{\Omega}, \quad e_{ij}(\mathbf{x}) = M_{ijkl}(\mathbf{x})e_{kl}^{\Omega}, \quad (7)$$

for both inside and outside of the inclusion, where

$$M_{ijkl}(\mathbf{x}) = \frac{1}{2} \left[ J_{ikl,j}(\mathbf{x}) + J_{jkl,i}(\mathbf{x}) \right], \tag{8}$$

$$J_{ikl}(\mathbf{x}) = \frac{1}{4\pi\rho\omega^2} \left\{ \lambda \delta_{kl} f_{imm}(\mathbf{x}, \alpha) + 2\mu [f_{ikl}(\mathbf{x}, \alpha) - f_{ikl}(\mathbf{x}, \beta)] \right\}$$

$$- \mu \beta^{2} [\delta_{ik} f_{,l}(\mathbf{x}, \beta) + \delta_{il} f_{,k}(\mathbf{x}, \beta)] \}, \quad (9)$$

$$f(\mathbf{x}, k) = \int_{\Omega} \frac{e^{ikr}}{r} d\mathbf{x}'.$$
 (10)

Mikata and Nemat-Nasser (1990) called  $M_{ijkl}(\mathbf{x})$  in Eq. (8) the dynamic Eshelby tensor. The expression in Eq. (9) slightly differs from that given by Mikata and Nemat-Nasser (1990) since we have used

$$f_{imm}(\mathbf{x},\,\beta) + \beta^2 f_{,i}(\mathbf{x},\,\beta) = 0 \tag{11}$$

to simplify (9). For a spherical inclusion, Mikata and Nemat-Nasser (1990) evaluated the integral (10) in closed form and hence computed the exact dynamic Eshelby tensor. Here we evaluate this integral for an infinitely long circular cylindrical inclusion  $\Omega$ :  $x_1^2 + x_2^2 < a^2$  and  $-\infty < x_3 < \infty$ , and then find the corresponding Eshelby tensor. To do this, we recall the following formulas (Gradshteyn and Ryzhik, 1965).

#### (a) Integral formula.

$$\int_{-\infty}^{\infty} \frac{e^{ikr}}{r} dx'_{3} = i\pi H_{0}^{(1)}(kR), \qquad (12)$$

$$R^{2} = (x_{\alpha} - x_{\alpha}')(x_{\alpha} - x_{\alpha}') = z^{2} + z'^{2} - 2zz' \cos \theta, \quad (13)$$

$$z^{2} = x_{\alpha}x_{\alpha}, \quad z'^{2} = x'_{\alpha}x'_{\alpha}, \quad \cos \theta = \frac{x_{\alpha}x'_{\alpha}}{zz'}.$$
 (14)

(b) Addition theorem.

 $H_{0}^{(1)}(kR)$ 

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$$= \begin{cases} J_{0}(kz)H_{0}^{(1)}(kz') + 2\sum_{M=1}^{\infty} J_{M}(kz)H_{M}^{(1)}(kz') \cos M\theta, \\ (z < z') \\ J_{0}(kz')H_{0}^{(1)}(kz) + 2\sum_{M=1}^{\infty} J_{M}(kz')H_{M}^{(1)}(kz) \cos M\theta, \\ (z > z') \end{cases}$$
(15)

#### (c) Recurrence relations

1

$$\frac{d}{dz}[zJ_1(z)] = zJ_0(z), \frac{d}{dz}[zH_1^{(1)}(z)] = zH_0^{(1)}(z).$$
(16)

Here  $J_M(z)$  is the Bessel function of order *M* and  $H_M^{(1)}(z)$  is the Hankel function of the first kind of order *M*.

Based on the formulas (12), (15), and (16), the integral (10) can now be calculated for a circular cylindrical inclusion.

$$f(\mathbf{x}, k) = \begin{cases} \left( \int_{0}^{z} z' dz' + \int_{z}^{a} z' dz' \right) \int_{0}^{2\pi} d\theta \int_{-\infty}^{\infty} dx'_{3} \frac{e^{ikr}}{r}, \\ \mathbf{x} \in \Omega \\ \int_{0}^{a} z' dz' \int_{0}^{2\pi} d\theta \int_{-\infty}^{\infty} dx'_{3} \frac{e^{ikr}}{r}, \quad \mathbf{x} \in R^{3} - \Omega \end{cases}$$
$$= \frac{2\pi^{2}i}{k} \begin{cases} zJ_{1}(kz)H_{0}^{(1)}(kz) + aJ_{0}(kz)H_{1}^{(1)}(ka) \\ -zJ_{0}(kz)H_{1}^{(1)}(kz), \quad \mathbf{x} \in \Omega \\ aJ_{1}(ka)H_{0}^{(1)}(kz), \quad \mathbf{x} \in R^{3} - \Omega \end{cases}$$
(17)

Furthermore, by using

$$J_0(kz)H_1^{(1)}(kz) - J_1(kz)H_0^{(1)}(kz) = -\frac{2i}{\pi kz},$$
 (18)

(17) can be simplified to

$$f(\mathbf{x}, k) \equiv N(z, k) = -4\pi \left[\frac{1}{k^2}\Lambda(\Omega) + \Phi(k)\Psi_0(kz)\right], \quad (19)$$

where

$$\Phi(k) = \begin{cases} -\frac{i\pi a}{2k} H_1^{(1)}(ka), & \mathbf{x} \in \Omega \\ -\frac{i\pi a}{2k} J_1(ka), & \mathbf{x} \in R^3 - \Omega \end{cases},$$
$$\Psi_0(kz) = \begin{cases} J_0(kz), & \mathbf{x} \in \Omega \\ H_0^{(1)}(kz), & \mathbf{x} \in R^3 - \Omega \end{cases}.$$
(20)

Thus, the exact steady-state Eshelby tensor for an infinite circular cylindrical inclusion is readily obtained from Eqs. (8), (9), and (19). As can be seen from these equations, unlike for the quasi-static problem (Eshelby, 1957), the dynamic Eshelby tensor varies even within the inclusion. The calculation of the dynamic Eshelby tensor (8) requires the following expressions for the derivatives of the potential function  $f(\mathbf{x}, k)$ .

$$f_{,3}(\mathbf{x}, k) = 0, \quad f_{,\alpha}(\mathbf{x}, k) = x_{\alpha}DN,$$
$$f_{,\alpha\beta}(\mathbf{x}, k) = \delta_{\alpha\beta}DN + x_{\alpha}x_{\beta}D^{2}N,$$
$$f_{,\alpha\beta\omega}(\mathbf{x}, k) = (x_{\alpha}\delta_{\beta\omega} + x_{\beta}\delta_{\omega\alpha} + x_{\omega}\delta_{\alpha\beta})D^{2}N + x_{\alpha}x_{\beta}x_{\omega}D^{3}N,$$
$$f_{,\alpha\beta\omega\rho}(\mathbf{x}, k) = (\delta_{\alpha\beta}\delta_{\omega\rho} + \delta_{\alpha\omega}\delta_{\beta\rho} + \delta_{\alpha\rho}\delta_{\beta\omega})D^{2}N$$

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+ 
$$(x_{\alpha}x_{\beta}\delta_{\omega\rho} + x_{\alpha}x_{\omega}\delta_{\beta\rho} + x_{\alpha}x_{\rho}\delta_{\beta\omega} + x_{\beta}x_{\omega}\delta_{\alpha\rho}$$
  
+  $x_{\beta}x_{\rho}\delta_{\alpha\omega} + x_{\omega}x_{\rho}\delta_{\alpha\beta})D^{3}N + x_{\alpha}x_{\beta}x_{\omega}x_{\rho}D^{4}N$ , (21)

where D = d/(zdz) and

$$D^{l}N = -4\pi \left(-\frac{k}{z}\right)^{l} \Phi(k)\Psi_{l}(kz), \ (l \ge 1),$$

$$\Psi_{l}(kz) = \left(-\frac{z}{k}\right)^{l} D^{l}\Psi_{0}(kz), \ (l \ge 1),$$

$$\Psi_{l}(kz) = \begin{cases} J_{l}(kz), & \mathbf{x} \in \Omega \\ H_{l}^{(1)}(kz), & \mathbf{x} \in R^{3} - \Omega \end{cases},$$

$$(l = 0, 1, 2, ...), \text{ no sum on } l. (22)$$

#### **3** Quasi-static Deformations

The classical Eshelby tensor  $S_{ijkl}$  for quasi-static deformations can be recovered from the present dynamic Eshelby tensor (8) by taking the limit  $\omega \rightarrow 0$ , i.e.,

$$S_{ijkl}(\mathbf{x}) = \lim_{\omega \to 0} M_{ijkl}(\mathbf{x}) = \frac{1}{2} \left[ J_{ikl,j}^{s}(\mathbf{x}) + J_{jkl,i}^{s}(\mathbf{x}) \right], \quad (23)$$

where

$$J_{ikl}^{S}(\mathbf{x}) = \lim_{\omega \to 0} J_{ikl}(\mathbf{x}) = \frac{\lambda + \mu}{\lambda + 2\mu} \psi_{,ikl}(\mathbf{x}) - \frac{\lambda}{\lambda + 2\mu} \delta_{kl} \phi_{,i}(\mathbf{x}) - \delta_{ik} \phi_{,l}(\mathbf{x}) - \delta_{il} \phi_{,k}(\mathbf{x}), \quad (24)$$

$$\psi(\mathbf{x}) = \frac{1}{4\pi} \int_{\Omega} r d\mathbf{x}', \ \phi(\mathbf{x}) = \frac{1}{4\pi} \int_{\Omega} \frac{1}{r} d\mathbf{x}'.$$
(25)

Note that the two integrals (25) over an infinite circular cylinder diverge. However, the derivatives of the potential functions  $\psi(\mathbf{x})$ and  $\phi(\mathbf{x})$  appearing in (24) converge. The derivatives of  $\psi(\mathbf{x})$  and  $\phi(\mathbf{x})$  can be calculated in the same form as the derivatives of f in (21). Since a detailed discussion on  $\psi(\mathbf{x})$  and  $\phi(\mathbf{x})$  for a general ellipsoidal inclusion has been given by Mura (1982), only the relevant results for an infinite circular cylindrical inclusion are given below.

$$D^{2}\psi = \begin{cases} -\frac{1}{4}, & \mathbf{x} \in \Omega \\ -\frac{a^{2}}{2z^{2}} + \frac{a^{4}}{4z^{4}}, & \mathbf{x} \in R^{3} - \Omega \end{cases},$$
$$D\phi = \begin{cases} -\frac{1}{2}, & \mathbf{x} \in \Omega \\ -\frac{a^{2}}{2z^{2}}, & \mathbf{x} \in R^{3} - \Omega \end{cases}$$
(26)

By using (26), and recalling  $S_{ijkl} = S_{jikl} = S_{ijlk}$ , the nonzero components of the classical Eshelby tensor can be expressed as

$$S_{\omega\rho\alpha\beta} = \frac{4\nu - 1}{8(1 - \nu)} \,\delta_{\alpha\beta}\delta_{\omega\rho} + \frac{3 - 4\nu}{8(1 - \nu)} \,(\delta_{\alpha\omega}\delta_{\beta\rho} + \delta_{\alpha\rho}\delta_{\beta\omega}),$$

$$S_{3\rho3\beta} = \frac{1}{4} \delta_{\beta\rho}, \quad S_{\omega\rho33} = \frac{\nu}{2(1-\nu)} \delta_{\omega\rho}, \tag{27}$$

for the inside of the circular cylinder, and

$$S_{\omega\rho\alpha\beta} = \frac{a^2}{4} \left\{ D_{\omega\rho\alpha\beta} - \frac{1}{1-\nu} \left[ A_{\omega\rho\alpha\beta} \left( \frac{1}{z^2} - \frac{a^2}{2z^4} \right) - 2B_{\omega\rho\alpha\beta} \left( \frac{1}{z^4} - \frac{a^2}{z^6} \right) + 4C_{\omega\rho\alpha\beta} \left( \frac{2}{z^6} - \frac{3a^2}{z^8} \right) \right] \right\},$$

$$S_{3\rho3\beta} = \frac{a^2}{4z^2} \,\delta_{\beta\rho} - \frac{a^2}{2z^4} \,x_{\beta}x_{\rho},$$

$$S_{\omega\rho33} = \frac{\nu a^2}{2(1-\nu)} \left( \frac{1}{z^2} \,\delta_{\omega\rho} - \frac{2}{z^4} \,x_{\omega}x_{\rho} \right), \quad (28)$$

for the outside of the circular cylinder, where  $\nu$  is the Poisson ratio and

$$A_{\omega\rho\alpha\beta} = \delta_{\alpha\beta}\delta_{\omega\rho} + \delta_{\alpha\omega}\delta_{\beta\rho} + \delta_{\alpha\rho}\delta_{\beta\omega}$$

$$\begin{split} B_{\omega\rho\alpha\beta} &= x_{\alpha}x_{\beta}\delta_{\omega\rho} + x_{\alpha}x_{\omega}\delta_{\beta\rho} + x_{\alpha}x_{\rho}\delta_{\beta\omega} + x_{\beta}x_{\omega}\delta_{\alpha\rho} \\ &+ x_{\beta}x_{\rho}\delta_{\alpha\omega} + x_{\omega}x_{\rho}\delta_{\alpha\beta}, \end{split}$$

$$C_{\omega\rho\alpha\beta} = x_{\alpha}x_{\beta}x_{\omega}x_{\rho},$$

$$D_{\omega\rho\alpha\beta} = \frac{2}{z^2} \left( \frac{\nu}{1-\nu} \,\delta_{\alpha\beta}\delta_{\omega\rho} + \,\delta_{\alpha\omega}\delta_{\beta\rho} + \,\delta_{\alpha\rho}\delta_{\beta\omega} \right) \\ - \frac{2}{z^4} \left( \frac{2\nu}{1-\nu} \,x_\omega x_\rho \delta_{\alpha\beta} + \,x_\alpha x_\omega \delta_{\beta\rho} + \,x_\alpha x_\rho \delta_{\beta\omega} + \,x_\beta x_\omega \delta_{\alpha\rho} + \,x_\beta x_\rho \delta_{\alpha\omega} \right). \tag{29}$$

These expressions for the classical Eshelby tensor agree with those given in Mura (1982).

#### References

Cheng, Z. Q., and He, L. H., 1996, "Steady-State Response of a Cosserat Medium with a Spherical Inclusion," Acta Mechanica, Vol. 116, pp. 97-110.

Eshelby, J. D., 1957, "The Determination of the Elastic Field of an Ellipsoidal Inclusion, and Related Problems," *Proceedings of Royal Society*, Vol. A241, pp. 376–396.

Eshelby, J. D., 1959, "The Elastic Field Outside an Ellipsoidal Inclusion," Proceedings of Royal Society, Vol. A252, pp. 561-569.

Gradshteyn, I. S., and Ryzhik, I. M., 1965, Table of Integrals, Series, and Products, Academic Press, New York.

Mikata, Y., 1993, "Transient Elastic Field due to a Spherical Dynamic Inclusion with an Arbitrary Time Profile," *Quarterly Journal of Mechanics and Applied Mathematics*, Vol. 46, pp. 275–297.

Mikata, Y., and Nemat-Nasser, S., 1990, "Elastic Field due to a Dynamically Transforming Spherical Inclusion," ASME JOURNAL OF APPLIED MECHANICS, Vol. 57, pp. 845–849.

Mikata, Y., and Nemat-Nasser, S., 1991, "Interaction of a Harmonic Wave with a Dynamically Transforming Inhomogeneity," *Journal of Applied Physics*, Vol. 70, pp. 2071–2078.

Mura, T., 1982, *Micromechanics of Defects in Solids*, Martinus Nijhoff Publishers, Dordrecht, Netherlands.

Mura, T., 1988, "Inclusion Problems," ASME Applied Mechanics Reviews, Vol. 41, pp. 15-20.

Mura, T., Shodja, H. M., and Hirose, Y., 1996, "Inclusion Problems," ASME Applied Mechanics Reviews, Vol. 49, pp. S118-S127.

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